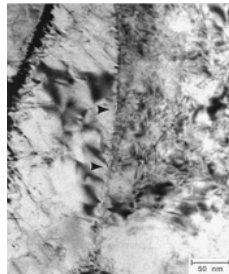
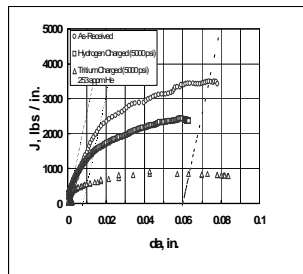
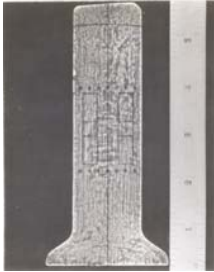


# Tritium Aging Effects on Forged Stainless Steel



**SRNL**<sup>TM</sup>  
SAVANNAH RIVER NATIONAL LABORATORY

**We Put Science To Work**

Michael Morgan

Materials Innovations in an  
Emerging Hydrogen Economy  
February 24-27, 2008  
Hilton Oceanfront | Cocoa Beach, Florida USA

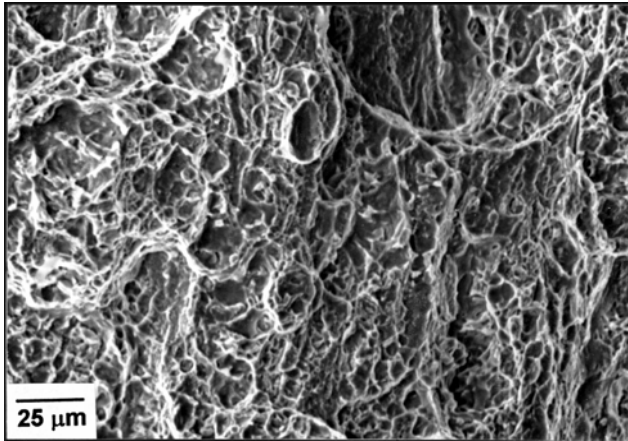
# Background

- Pressure vessels for tritium service are constructed from stainless steel forgings.
- Tritium and its decay product, helium, change the structural properties of stainless steels and make them more susceptible to cracking.
- Material and forging specifications have been developed for optimal material compatibility with tritium. They include: Composition, tensile properties, and select microstructural characteristics like grain size, flow line orientation, inclusion content, and ferrite distribution and content.
- For years, the forming process of choice was high-energy-rate forging (HERF)
- Today, some reservoir forgings are being made that use a conventional, more common process known as press forging (PF or CF).
- Conventional hydraulic or mechanical forging presses deform metal at 4-8 ft/s, about ten-fold slower than the HERF process.
- The material specifications continue to provide successful stockpile performance by ensuring that the two forging processes produce similar reservoir microstructures.

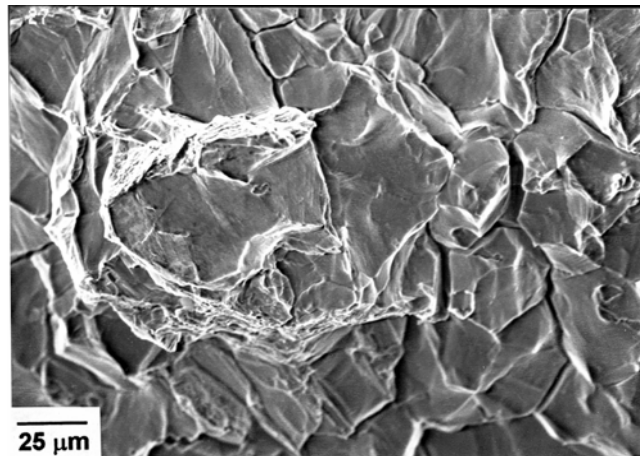
The purpose of this study was to measure and compare the fracture toughness properties of Type 21-6-9 stainless steel for:

- High-energy-rate and conventional forgings; in the
- Unexposed, hydrogen-exposed and tritium-exposed-and-aged conditions.

# Effect of Tritium Exposure on Stainless Steels



Unexposed

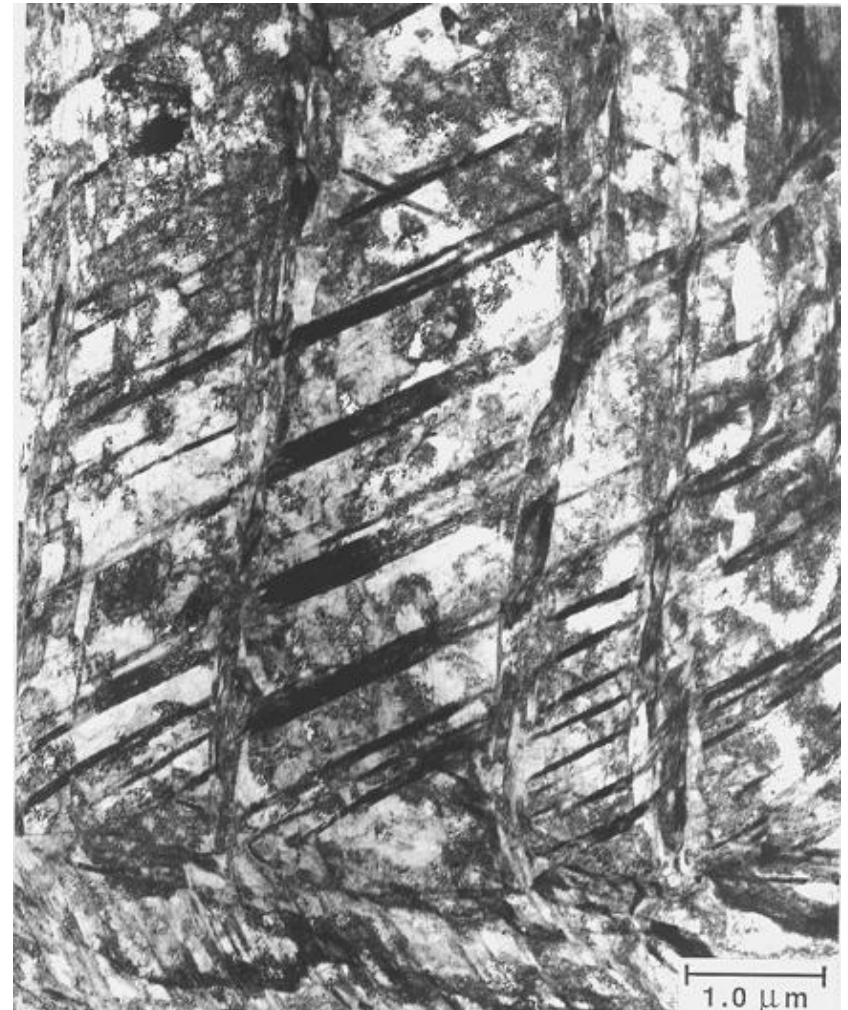
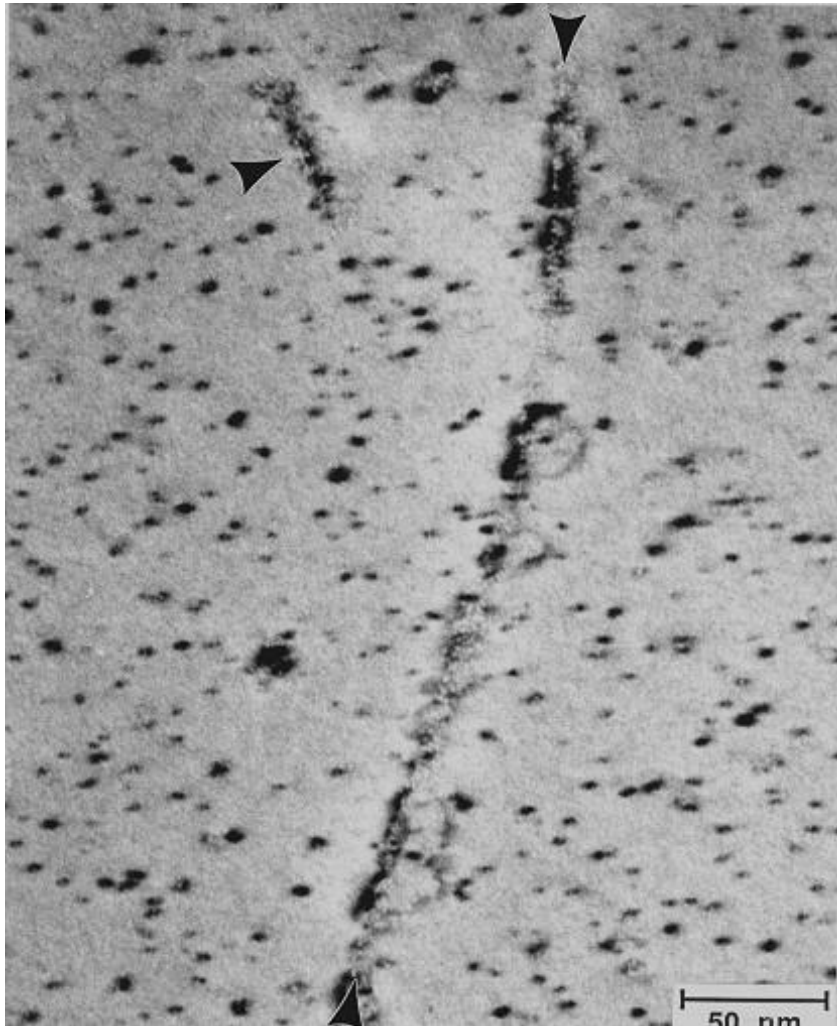


Tritium-Exposed & Aged





# Helium Hardened Microstructure



# Materials and Compositions

**Table I.** Compositions of Stainless Steel Forgings, Plates and Weld Filler Wires (Weight %)

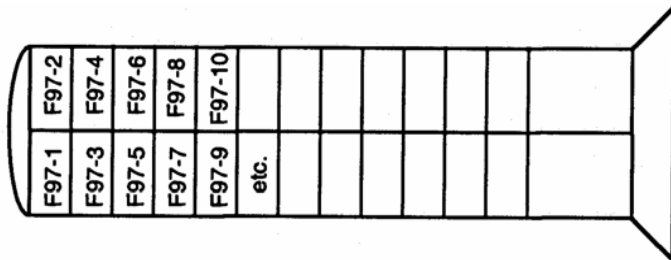
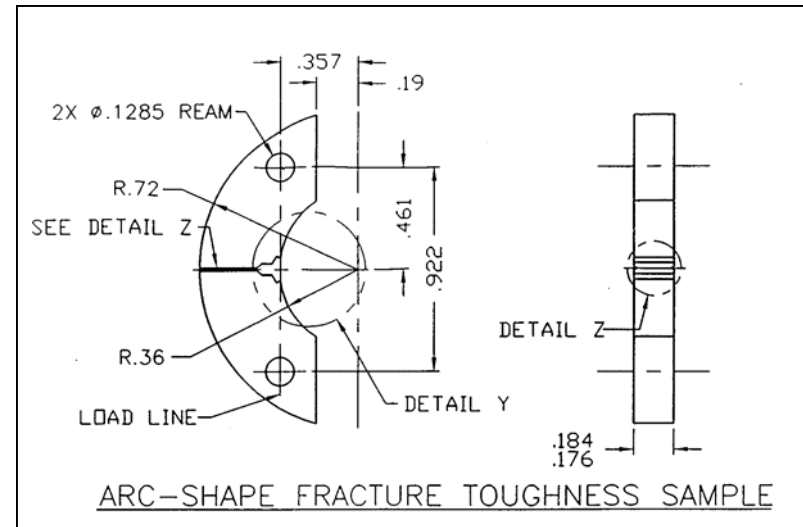
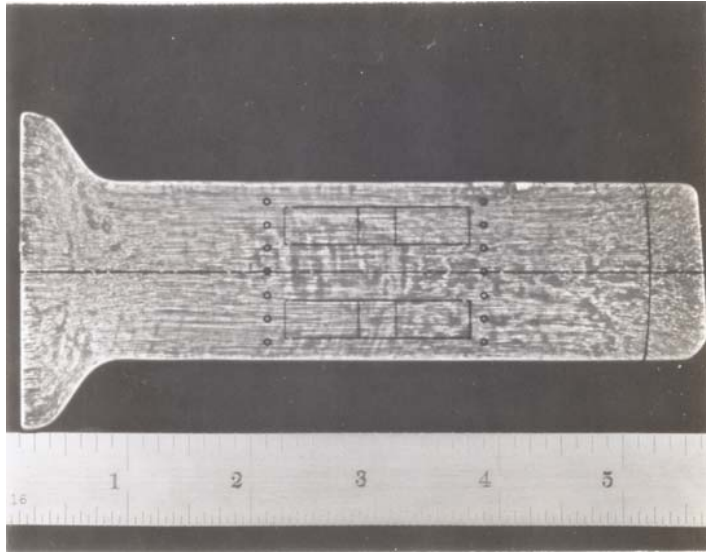
Material	Forging	Sample ID	Cr	Ni	Mn	P	Si	Co	Mo	C	S	N	O	Al	Cu
HERF*															
21-6-9	A4582	F97-X	19.4	6.4	8.5	0.021	0.33			0.04	<.001	0.28	0.0022	<.001	
CF**															
21-6-9	B7073	H94-X	19.1	6.7	9.9	0.01	0.41			0.03	0.004	0.28	0.001	0.005	
CF**															
21-6-9	B6275	F9-X	19.3	6.7	9.9	0.01	0.38			0.03	0.001	0.28	0.002	0.004	
Filler Wire	308L														
308L	Weldment	98-X	20.5	10.3	1.56	0.006	0.5	0.068	<0.01	0.028	0.012	0.055	-	-	0.015

\*High-Energy-Rate Forged

\*\*Conventionally Forged

Manufacturers' supplied compositions

# Forging and Sample Orientation



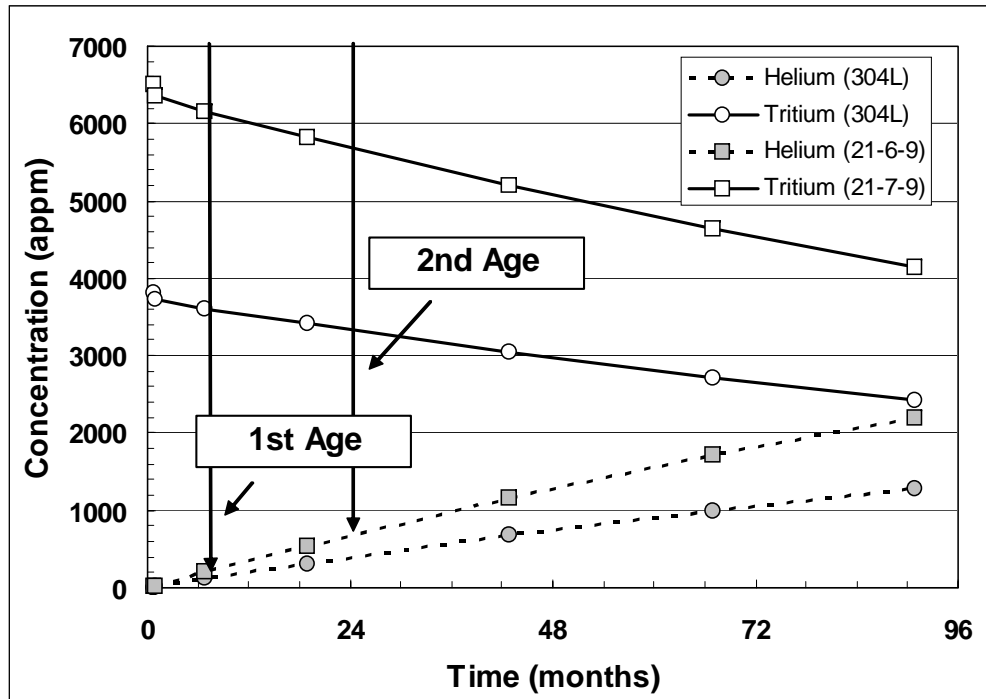
Forging A4582 -- 21-6-9 SS

# Mechanical Properties and Grain Size

Sample ID	Yield Strength psi	Ultimate Strength psi	% EL	Grain Size
F9 (CF)	87100	131400	48.3	10/7; 7 < 5%
H94 (CF)	99400	139300	44.3	10/7; 7 < 5%
F97 (HERF)	104800	139400	37.6	5/3

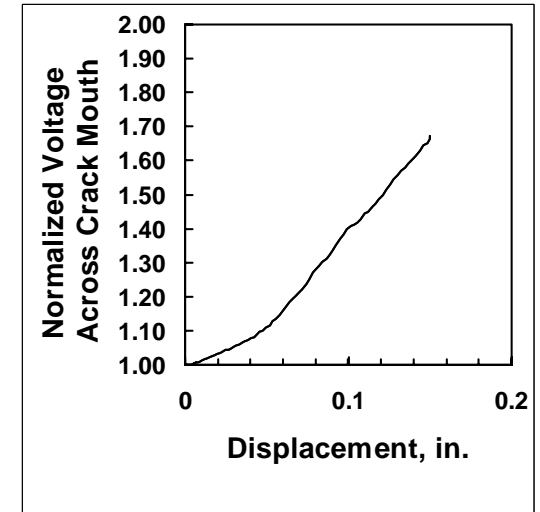
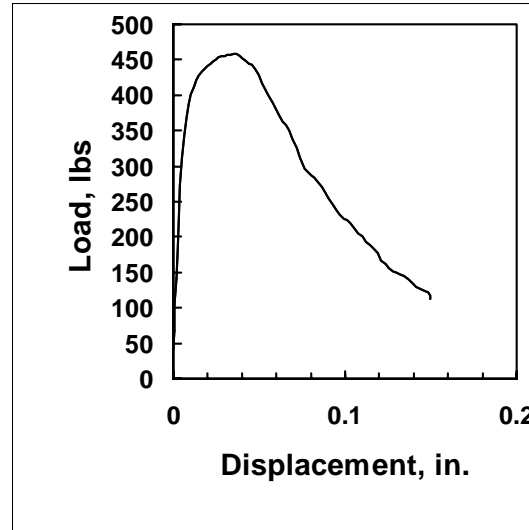


# Sample Cartridge and Aging Calculation

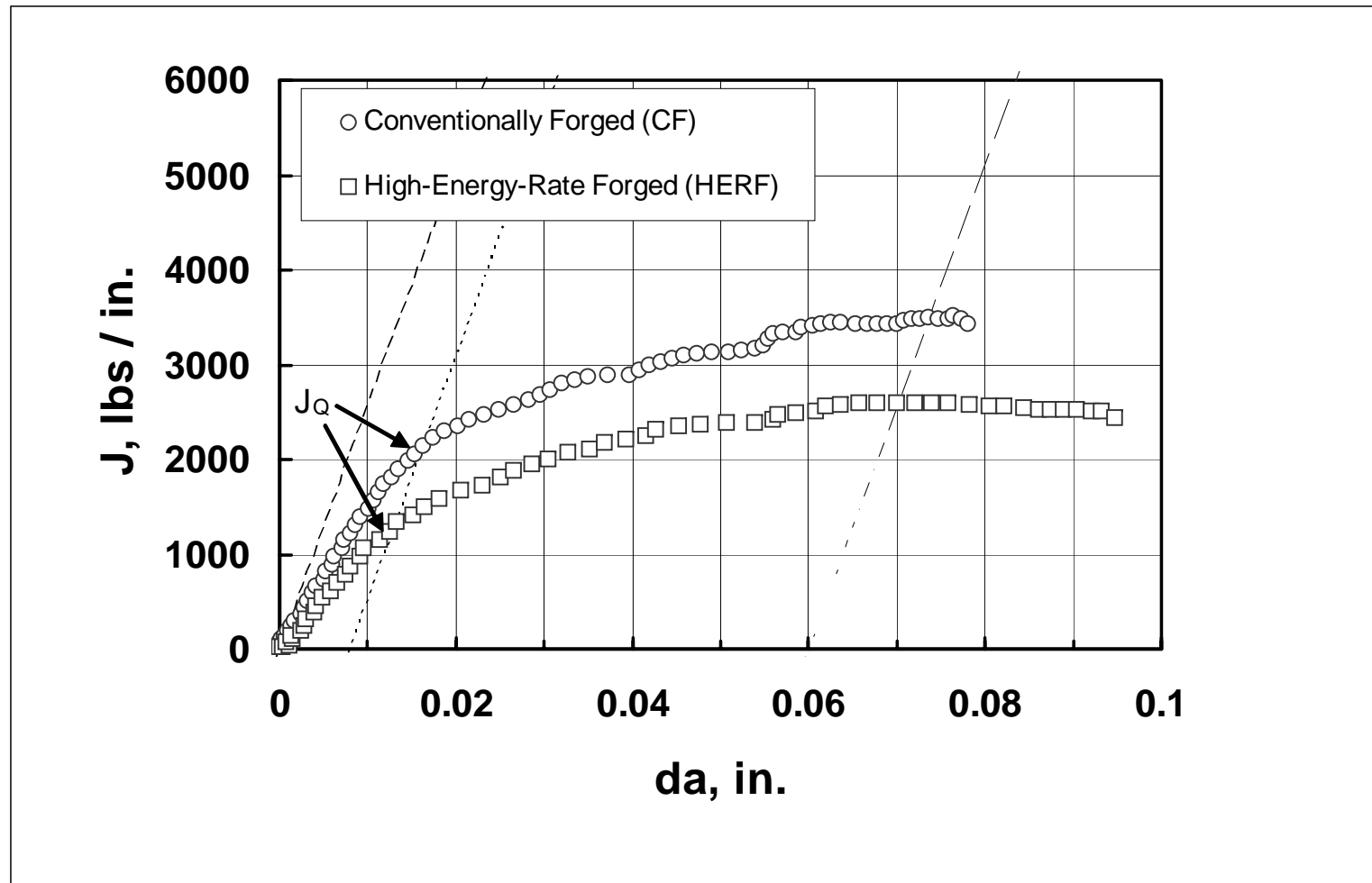


- Hydrogen and Tritium exposures conducted at 350 C for three weeks
- Tritium samples aged at -40C to build-in decay helium
- All samples were tested at ambient temperature in air

# Fracture Toughness Testing



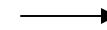
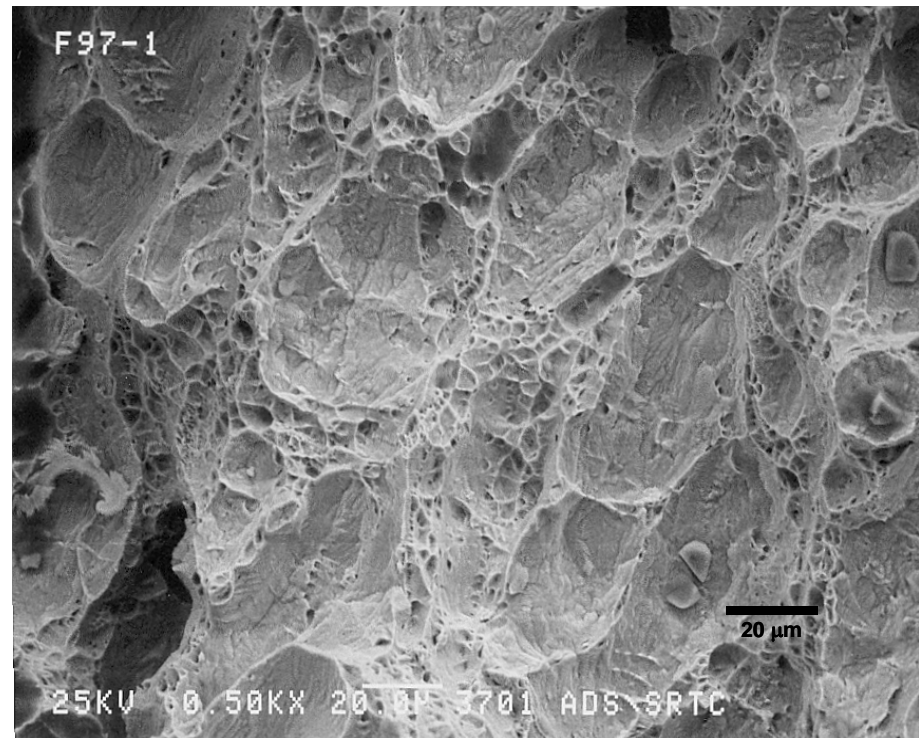
# J-R Curves for CF and HERF Steels



# Fracture Appearance Unexposed Heats



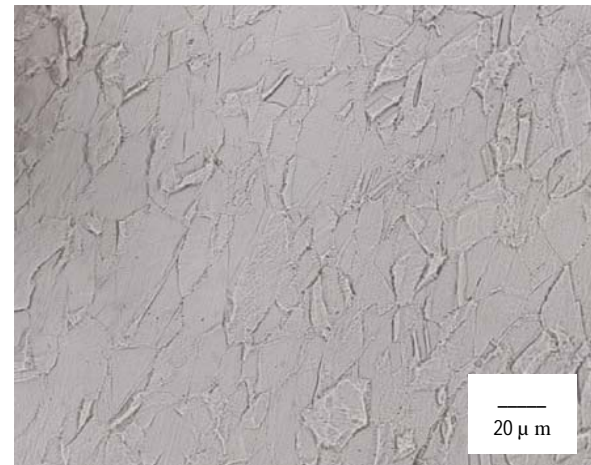
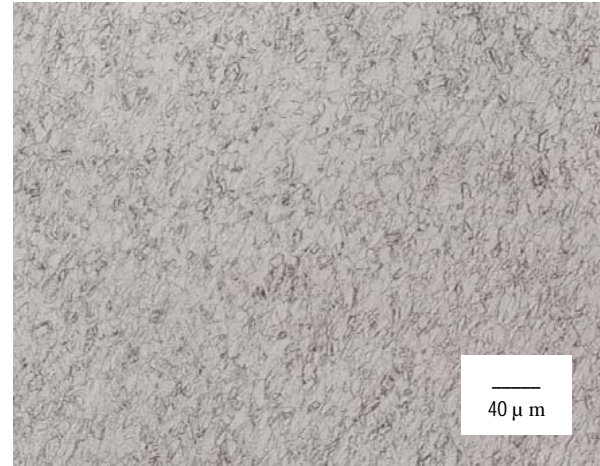
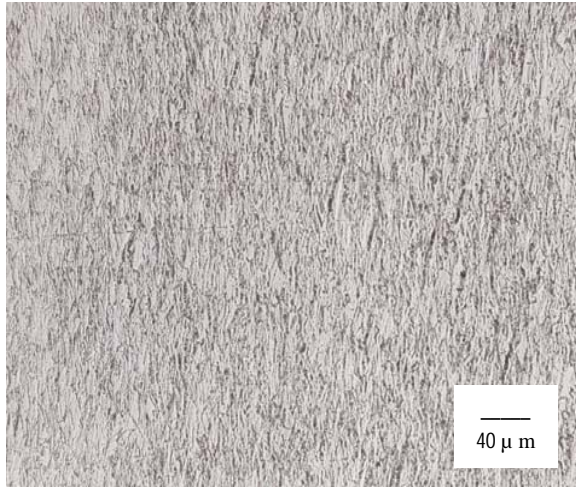
Conventionally Forged



High-Energy-Rate Forged



# Conventionally Forged Microstructures

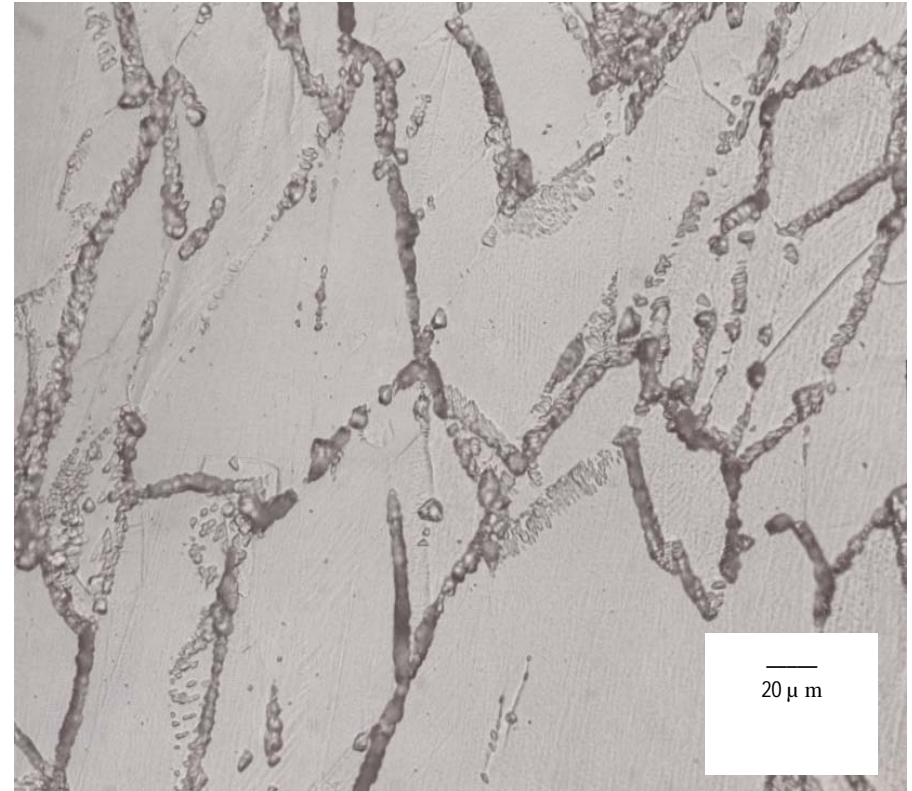


90 ksi Y.S. Heat

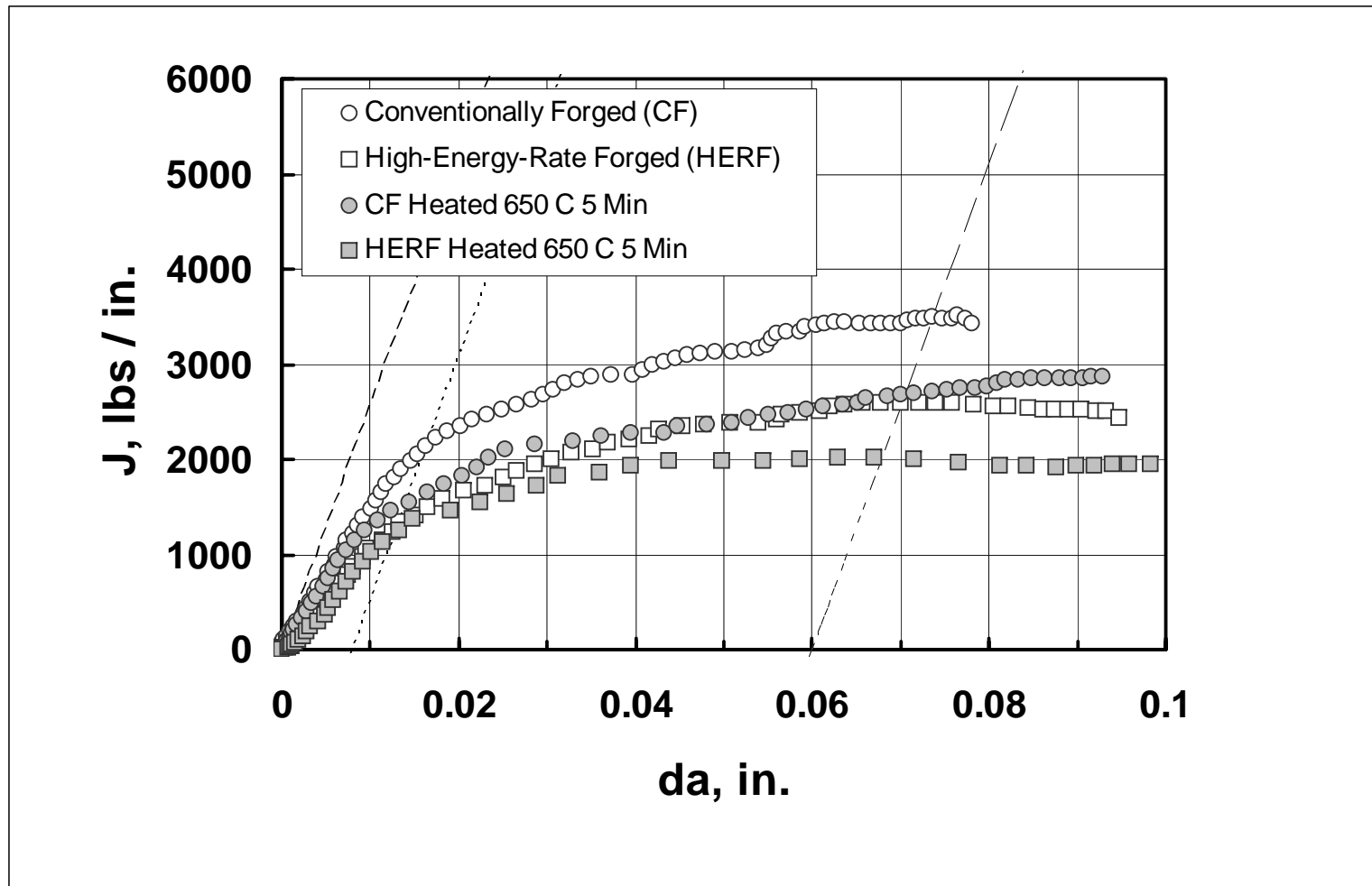
100 ksi Y.S. Heat



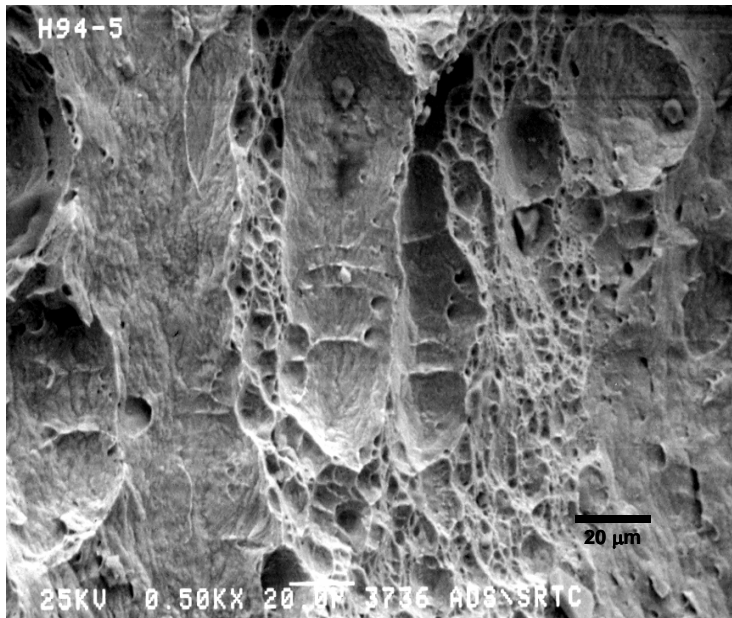
# HERF Microstructures



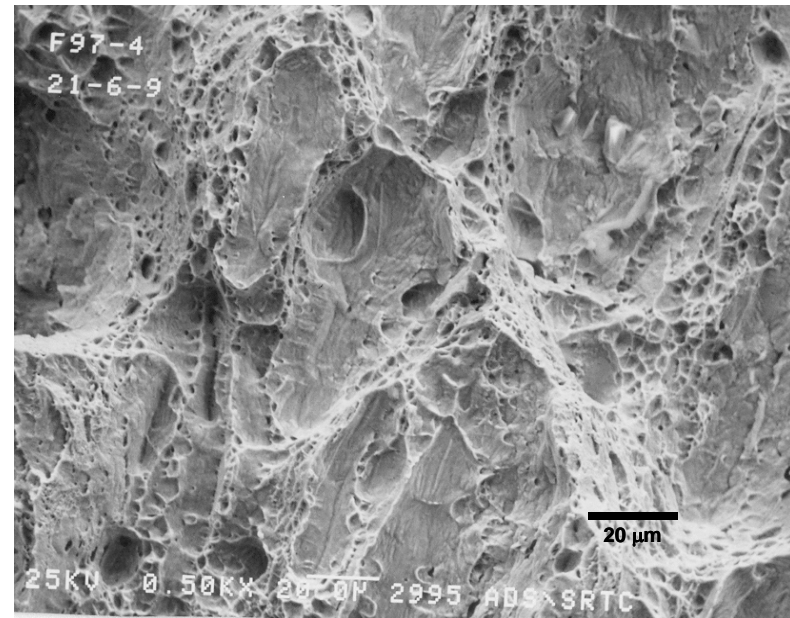
# J-R Curves for As-Received and Heat-Treated Steels



# Fracture Appearance Heat Treated Steels

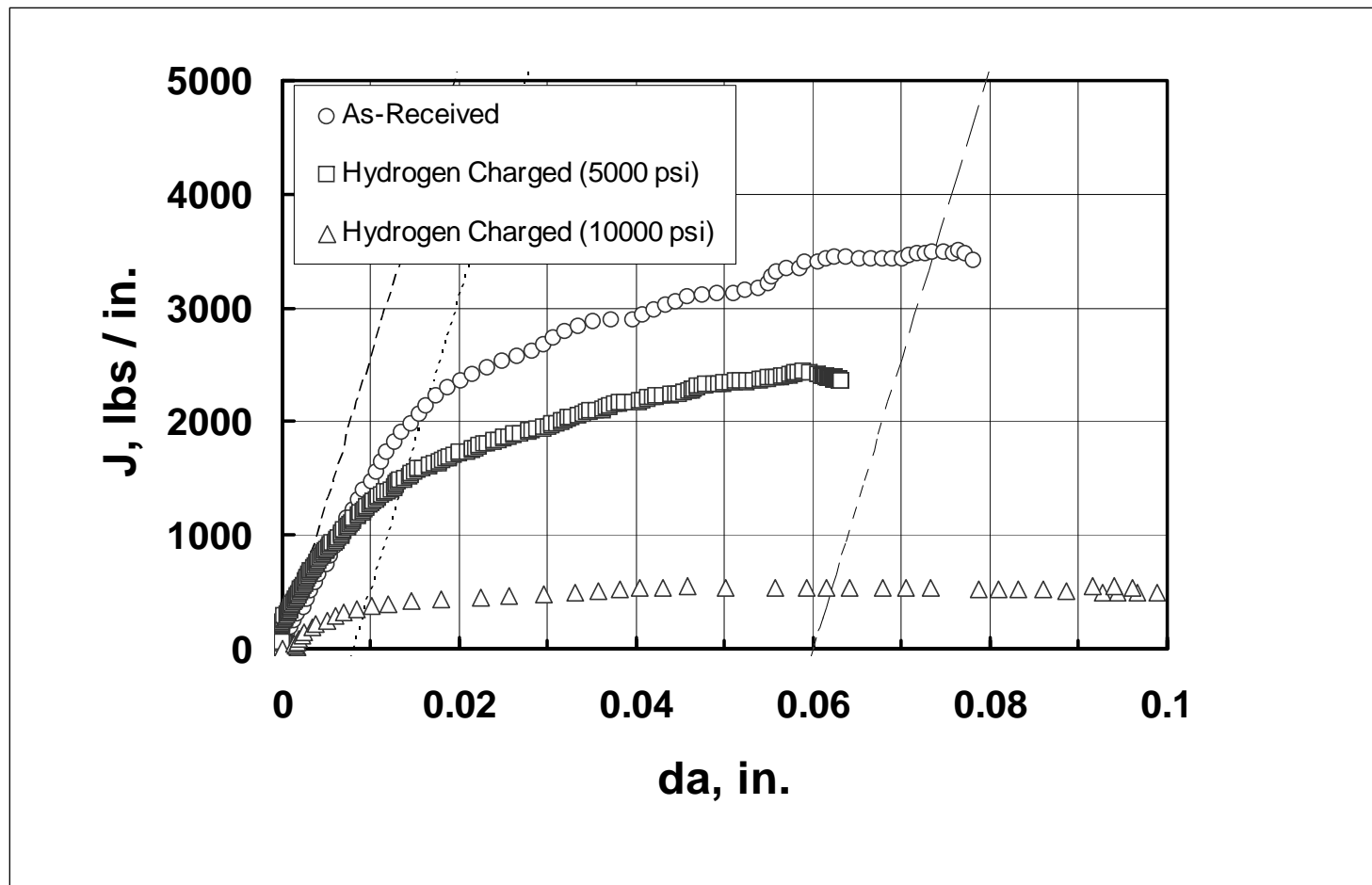


Conventionally Forged



High-Energy-Rate Forged

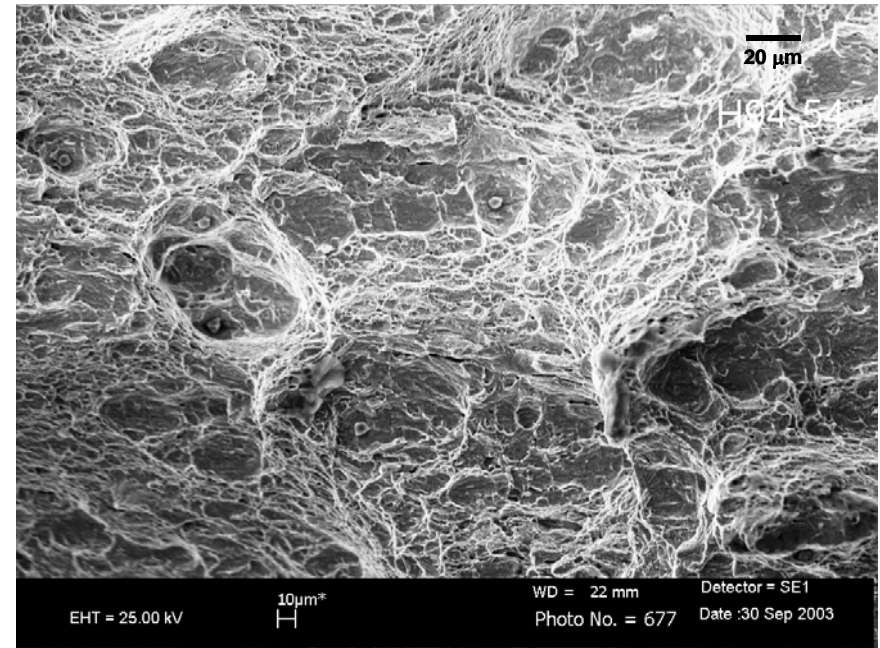
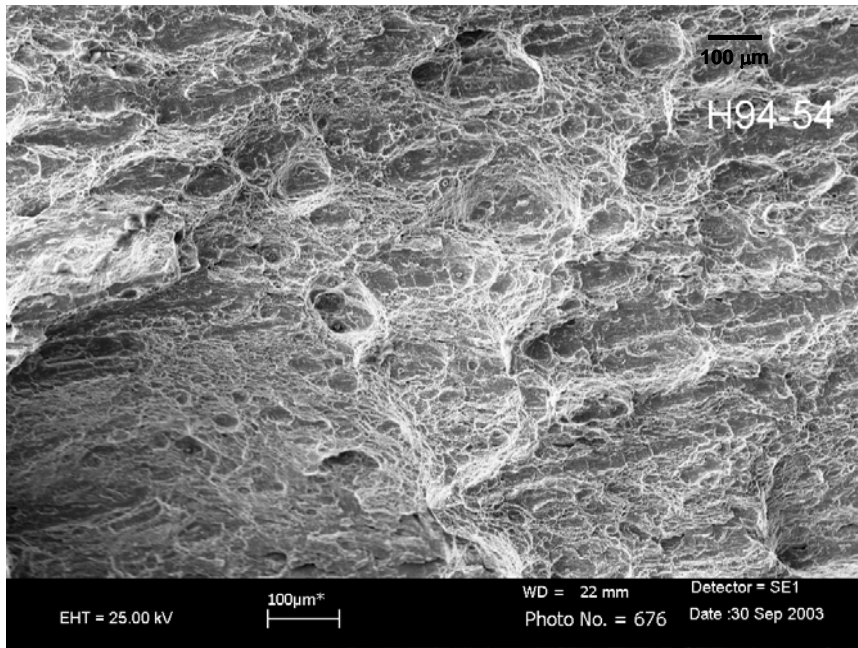
# Effect of Hydrogen Exposure on J-R Behavior



Conventionally Forged Type 21-6-9 Stainless Steel



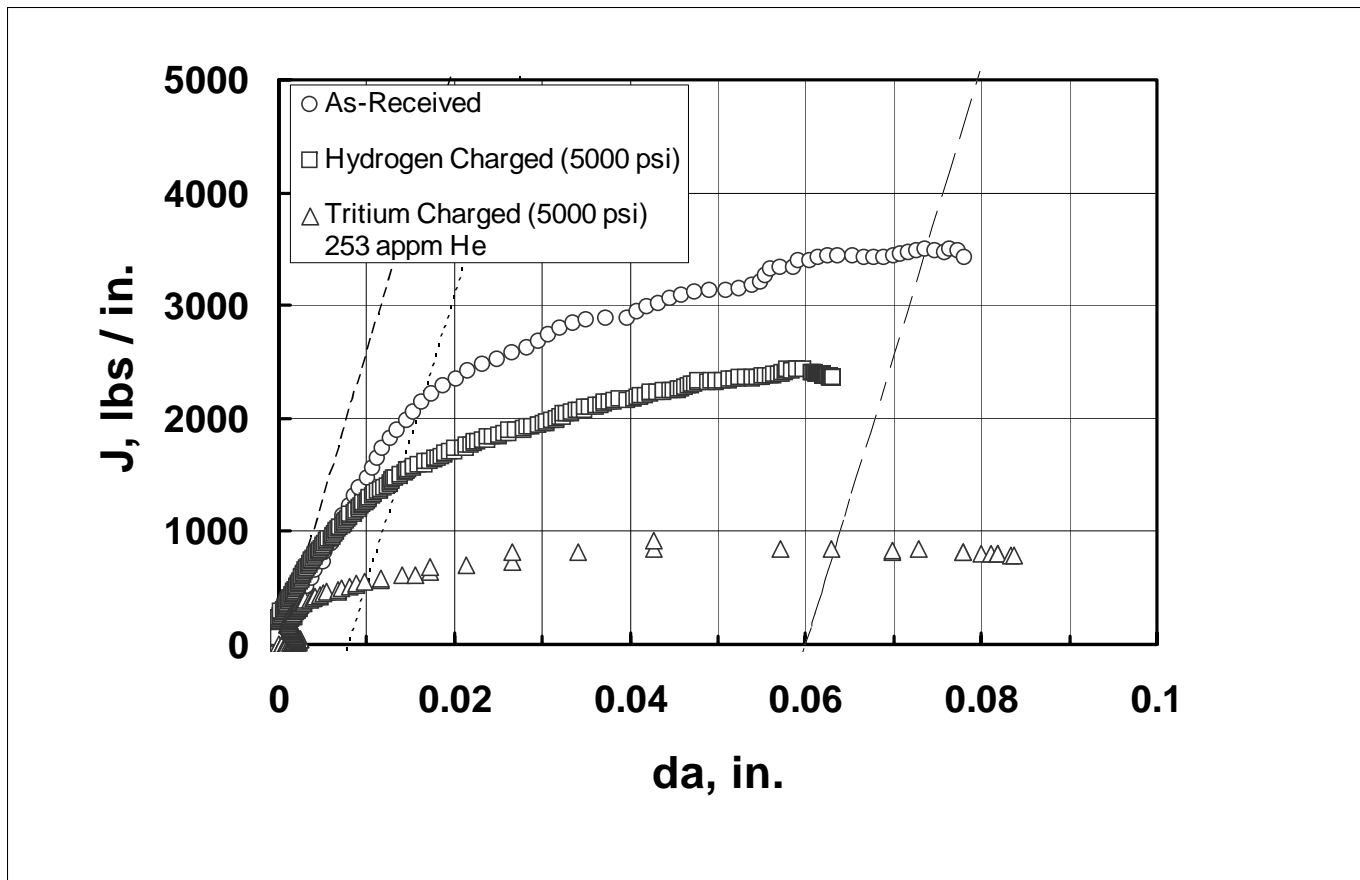
# Effect of Hydrogen on Fracture Appearance



Conventionally Forged Type 21-6-9 Stainless Steel

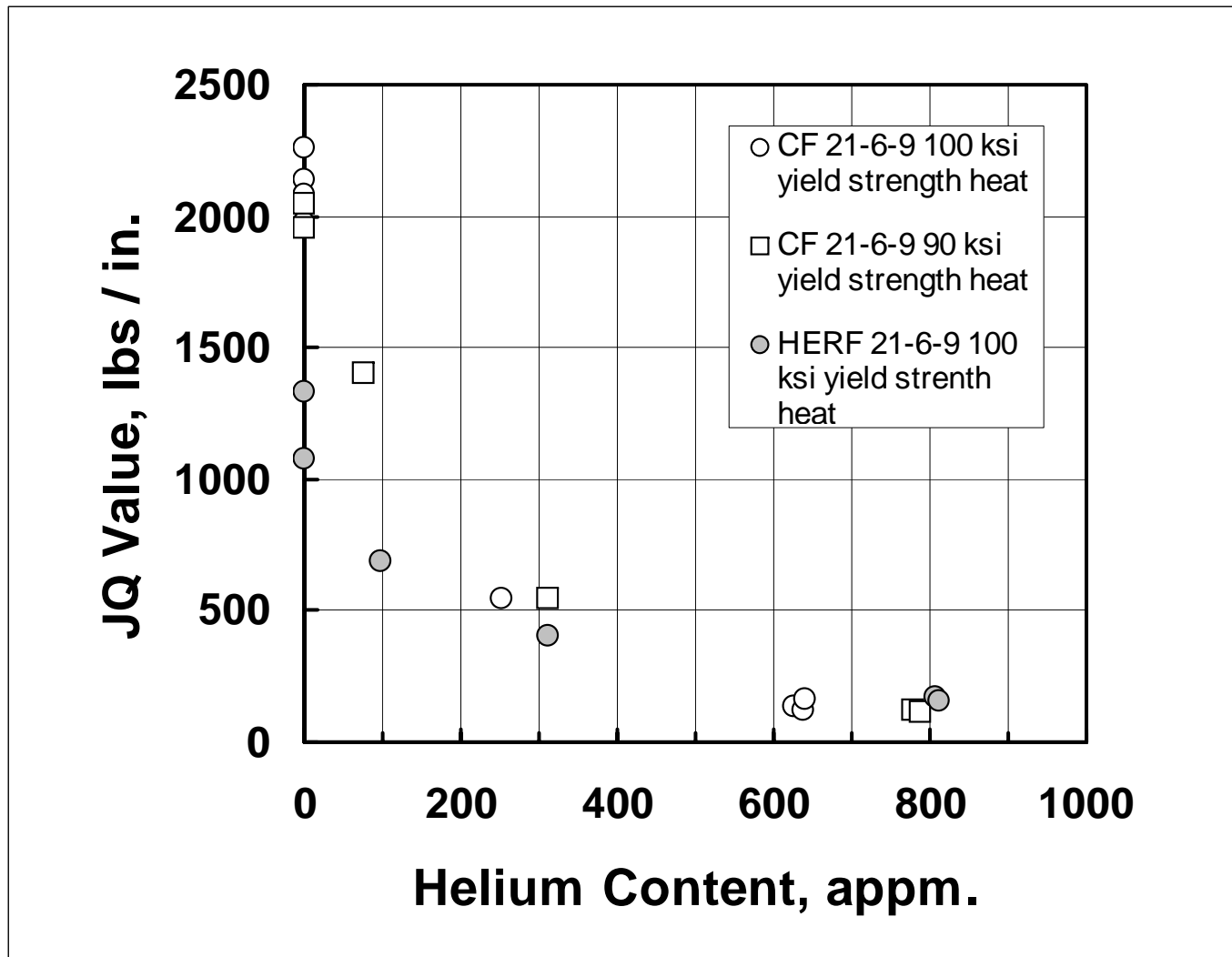


# Effect of Hydrogen, Tritium, and Decay Helium on J-R Behavior

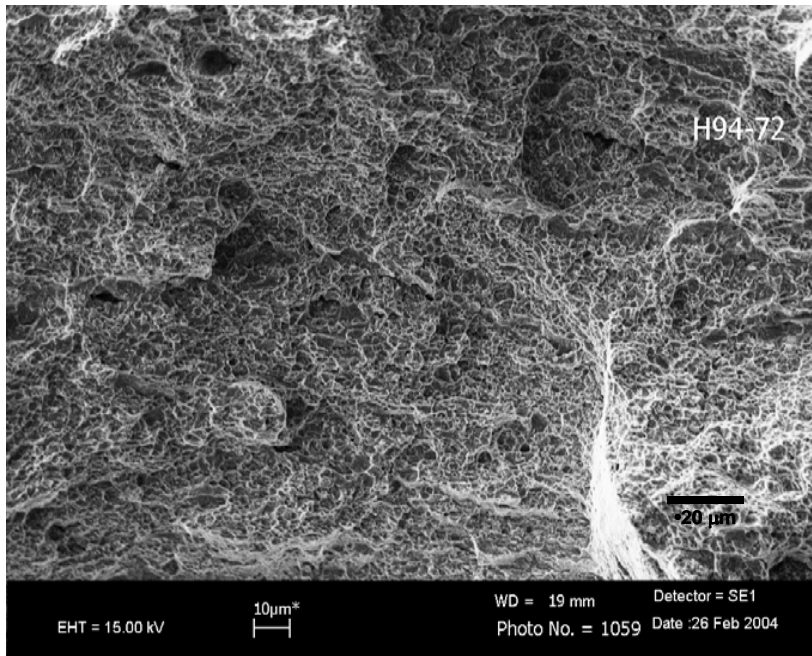


Conventionally Forged Type 21-6-9 Stainless Steel

# Effect of Decay Helium on Fracture Toughness

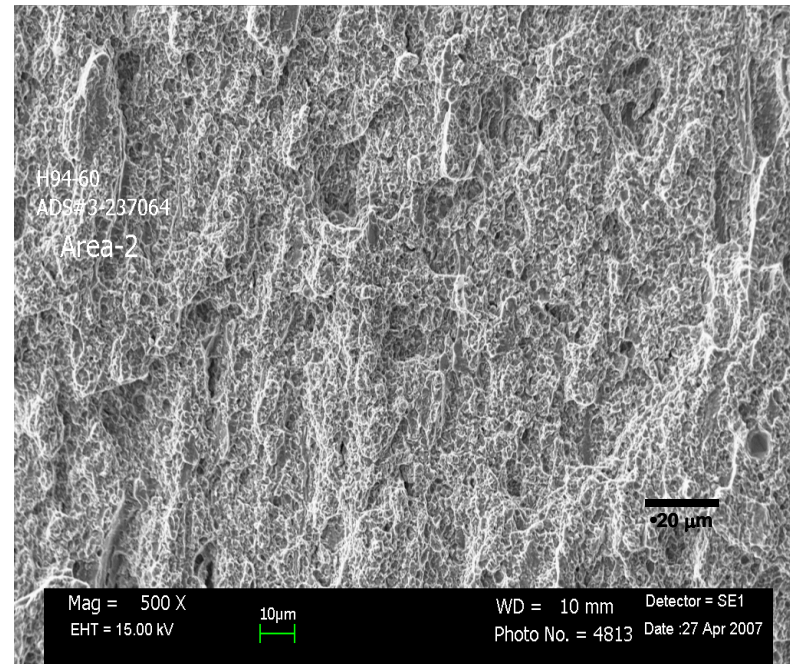


# Tritium Aging Effects on Fracture Appearance



↑

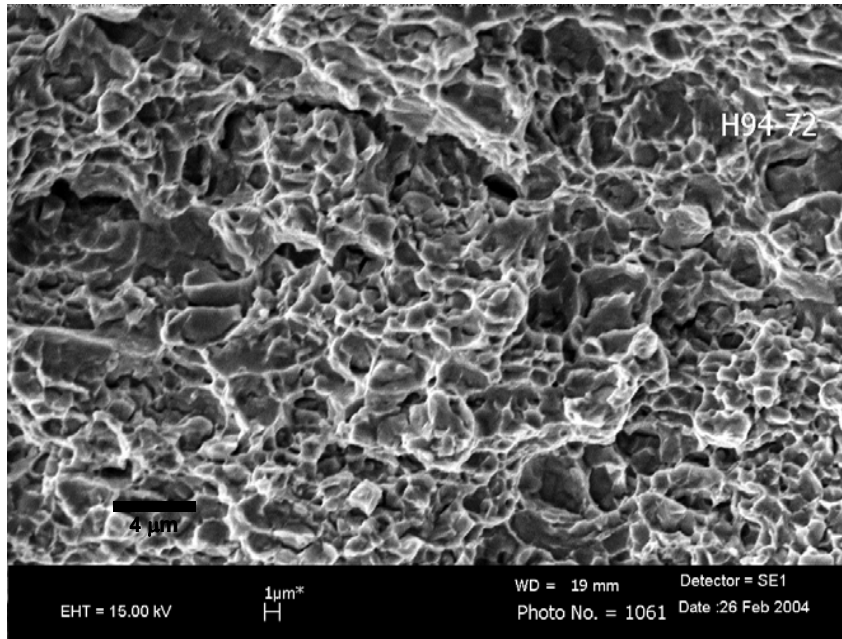
253 appm Helium



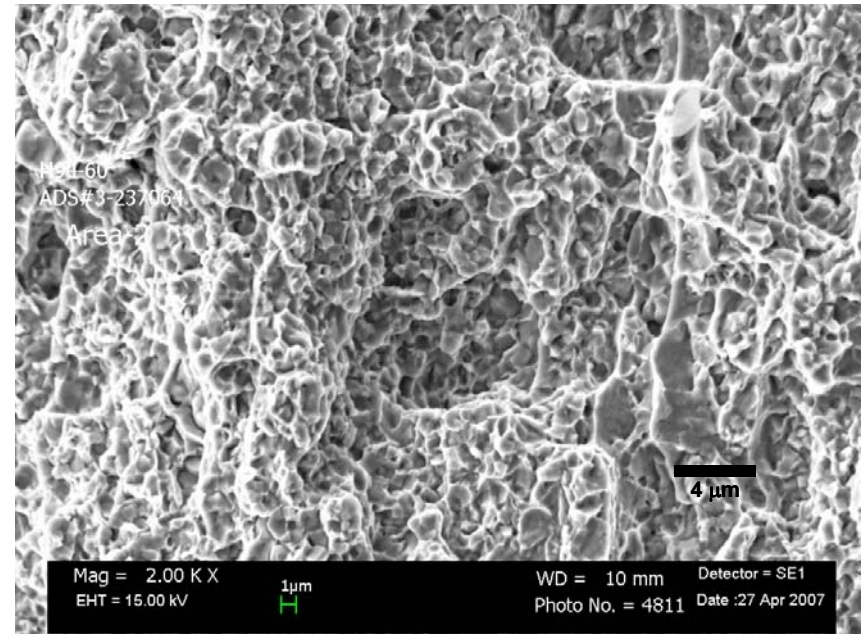
←

627 appm Helium

# Tritium Aging Effects on Fracture Appearance



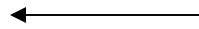
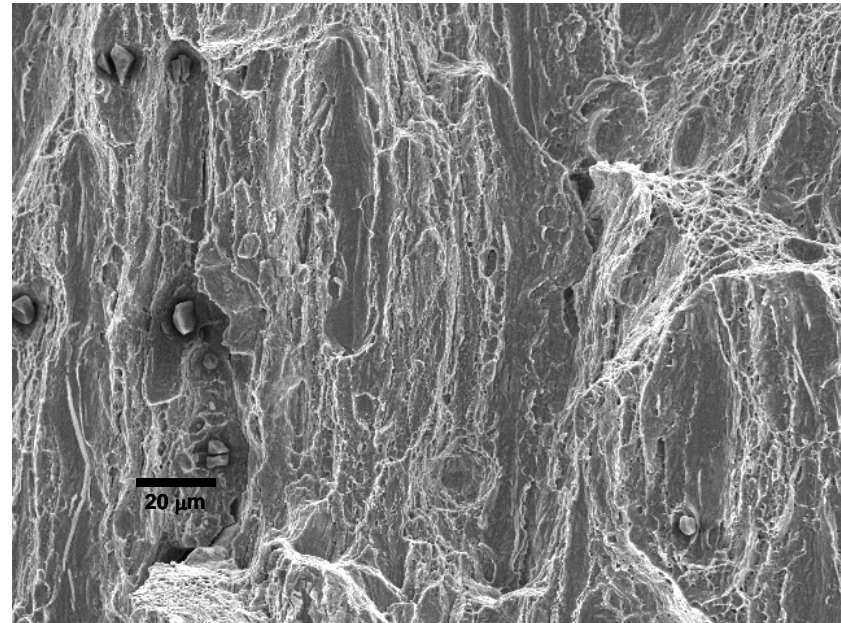
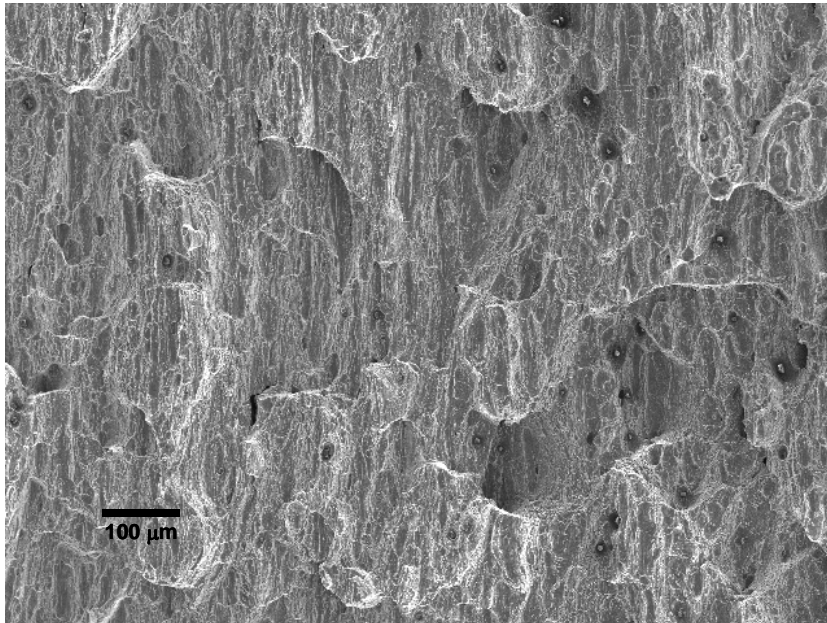
253 appm Helium



627 appm Helium



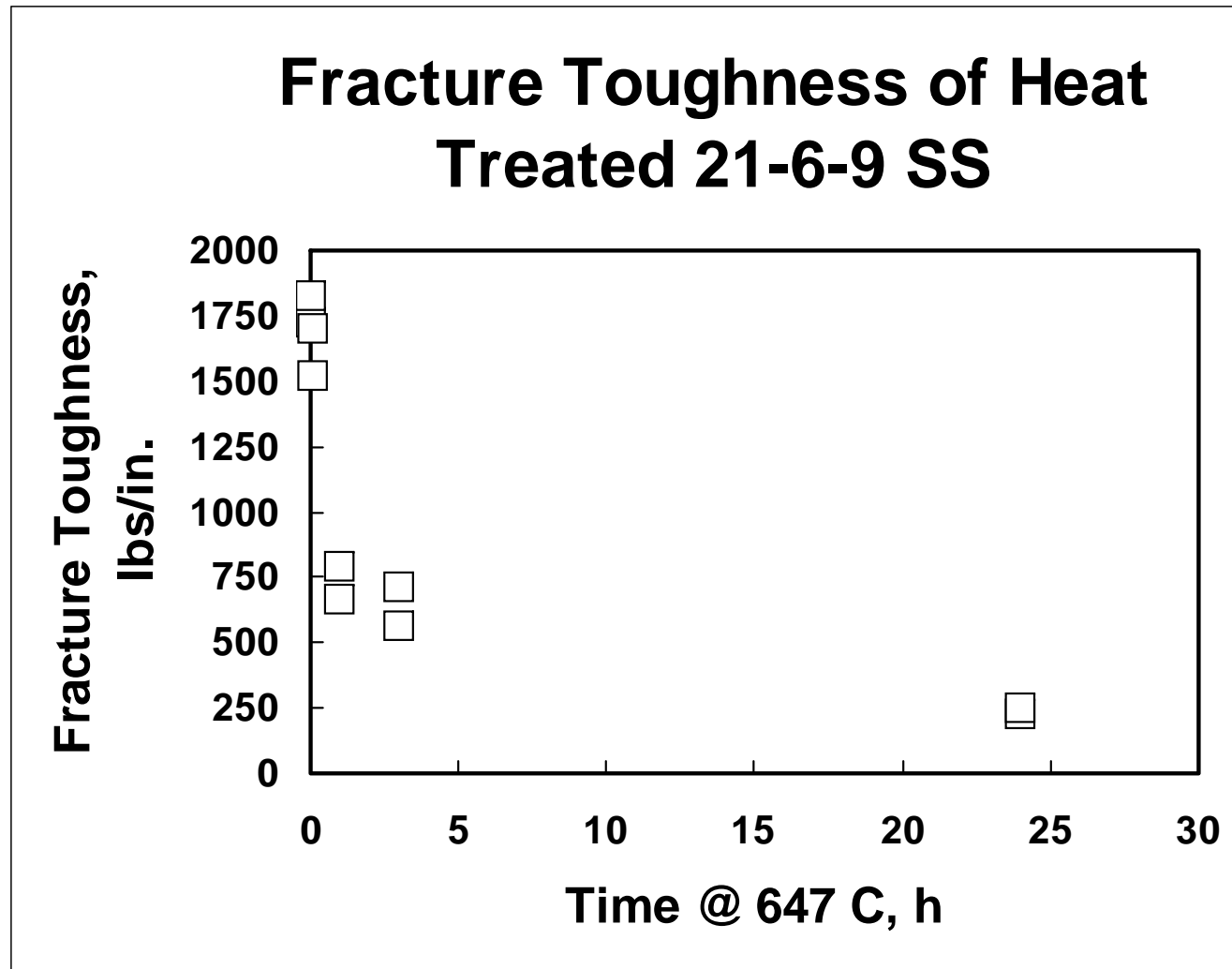
# Fracture Appearance of Tritium Exposed HERF Type 21-6-9 Stainless Steel



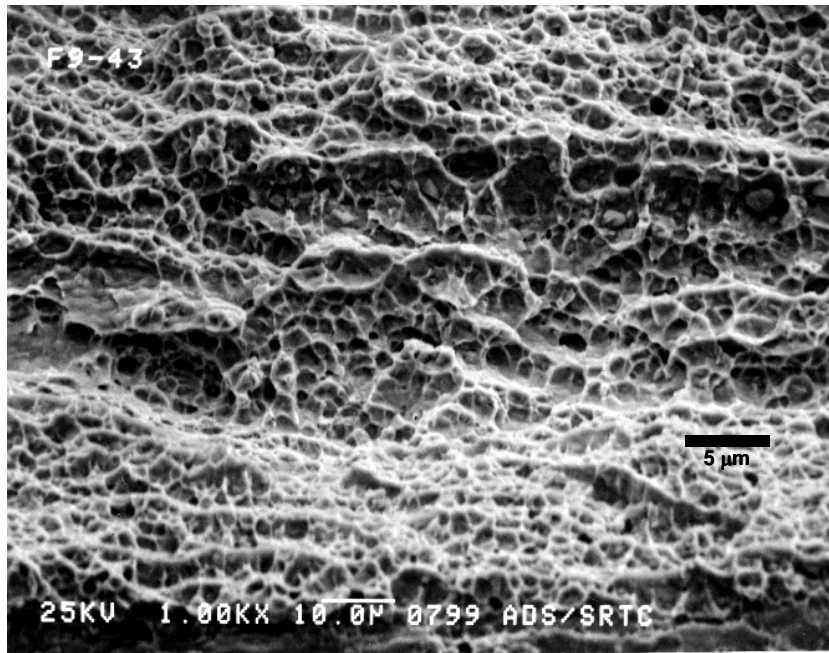
627 appm Helium



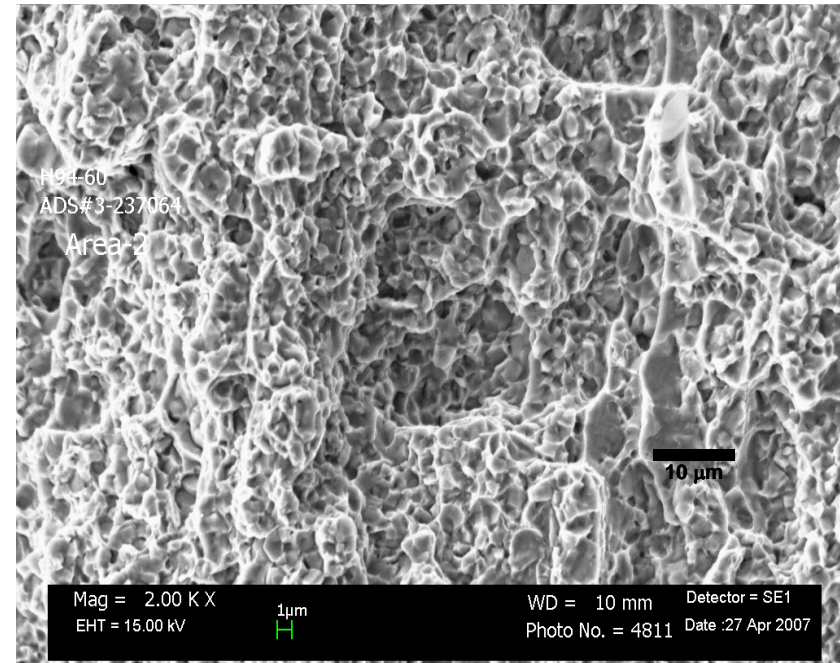
# Fracture Toughness - Heat Treated



# Comparison of Fracture Appearance – Heat Treated vs. Tritium-Exposed-and-Aged



Heat Treated 650 C 24 h



Tritium-Exposed-Aged for Seven  
Years (627 appm helium)

# Conclusions

- HERF Type 21-6-9 stainless steels had lower fracture toughness values than Conventionally Forged Type 21-6-9 steel because of its larger grain size and sensitization that occurred during the forging process.
- Hydrogen and tritium exposures lowered the JQ values and J-da curves. The degree of sensitization did not seem to affect the fracture toughness at high helium levels.
- Fracture modes of the forged steels were dominated by the dimpled rupture process in unexposed, hydrogen-exposed and tritium-exposed steels and welds.
- Heavily sensitized steels had a similar fracture appearance as tritium-exposed-and-aged steels